



TS

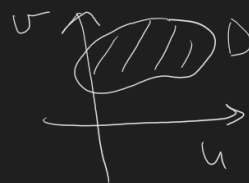


Previous lecture

surface $\leadsto$ parametrization

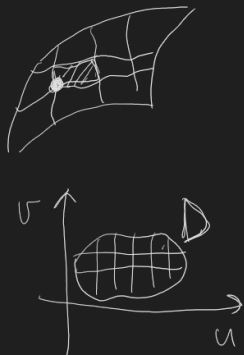
$$\vec{r}(u,v) = \langle x(u,v), y(u,v), z(u,v) \rangle$$

(u,v) is in D .



A normal vector to the surface
at $\vec{r}(u,v)$: $\vec{r}_u(u,v) \times \vec{r}_v(u,v)$.

Surface integrals of f -s:



$$\iint_S f(x,y,z) dS = \lim_{\Delta S_{ij} \rightarrow 0} \sum_{ij} f(\vec{r}(u_i, v_j)) \Delta S_{ij}$$

Formula for computation:

$$\iint_S f(x,y,z) dS = \iint_D f(\vec{r}(u,v)) |\vec{r}_u \times \vec{r}_v| dA$$

$$\text{Area of } S = \iint_S 1 dS$$

S is graph of $f-u$ a

$$\text{Area of } S = \iint_S 1 \, dS$$



In particular case when S is graph of f in g

$$\iint_S f(x, y, z) \, dS = \iint_D f(x, y, z(x, y)) \sqrt{1 + z_x^2 + z_y^2} \, dA$$

Surface integrals of vector fields.

Why one needs to integrate vector fields over surfaces:

Over curves:

work done by a force field
in moving a particle
along C $= \int_C \vec{F} \cdot d\vec{r}$

Over surfaces: consider a velocity field $\vec{F}$ of some fluid of density, say, 1.

The rate of flow through S , that is how much liquid goes through S per unit time is expressed by $\iint_S \vec{F} \cdot d\vec{S}$.





Same for heat flow, for electrical field...

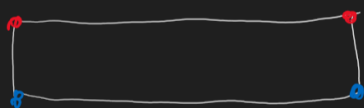


Will consider only "usual", 2-sided, surfaces.

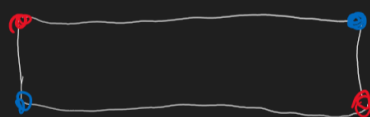


(called orientable.)

Möbius strip.

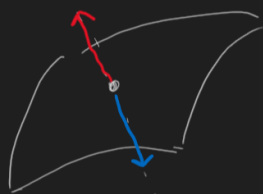


→ cylinder



→ Möbius strip.
(1-sided, or non-orientable, surface).

Will deal only with orientable surfaces.



At each pt there are 2 normal unit vectors.

A natural choice of a unit normal vector:

$$\vec{n} = \frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|}$$

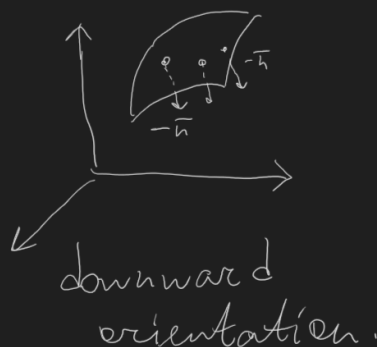
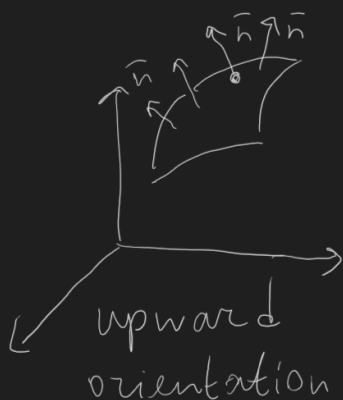


A natural choice of a unit normal vector

$$\bar{n} = \frac{\bar{r}_u \times \bar{r}_v}{|\bar{r}_u \times \bar{r}_v|}$$

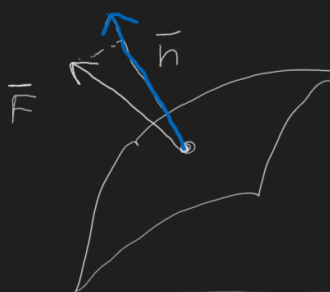
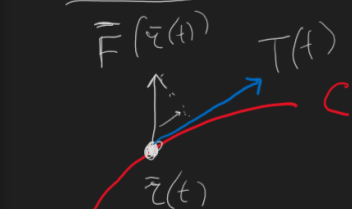
(The z^{nd} unit normal vector would be $-\bar{n}$)

In particular case when S is graph of a f-n g : $\bar{n} = \frac{\langle -g_x, -g_y, 1 \rangle}{|\langle -g_x, -g_y, 1 \rangle|}$



Curves

Surfaces



Def.

$$\int_C \bar{F} \cdot d\bar{r} = \int_C \bar{F} \cdot \bar{T} ds$$

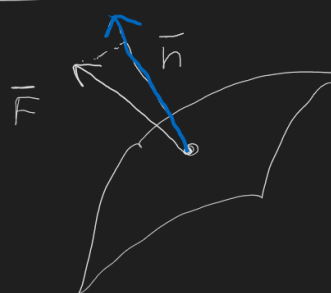
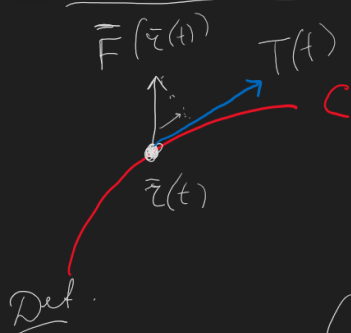
$$\iint_S \bar{F} \cdot d\bar{S} = \iint_S \bar{F} \cdot \bar{n} dS$$





Curves

Surfaces



Def.

$$\int_C \vec{F} \cdot d\vec{r} = \int_C (\vec{F} \cdot \vec{T}) ds$$

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_S \vec{F} \cdot \vec{n} dS$$



Motivation for taking $\vec{F} \cdot \vec{n}$:

in computing how much liquid goes through S , only normal component of velocity vectors matter.

Def. The surface integral of $\vec{F}$ over S is

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_S (\vec{F} \cdot \vec{n}) dS$$

It is also called the flux of F across S .



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It is also called the flux of $\vec{F}$
across S .

How to compute:

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_S (\vec{F} \cdot \vec{n}) dS$$

$$= \iint_D \left(\vec{F} \cdot \frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|} \right) |\vec{r}_u \times \vec{r}_v| dA$$

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_D \underbrace{\vec{F} \cdot (\vec{r}_u \times \vec{r}_v)}_{\text{dot product}} dA$$

Case when S is a graph! ^{of g}

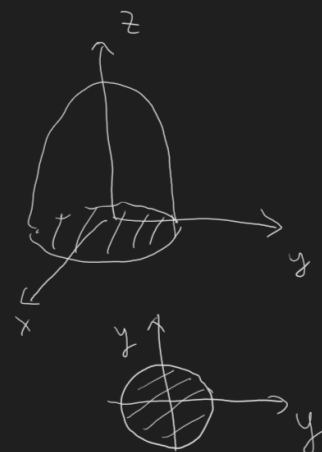
$$\vec{F} = \langle \underline{P}, \underline{Q}, \underline{R} \rangle, \quad \vec{r}_u \times \vec{r}_v = \langle \underline{-g_x}, \underline{-g_y}, 1 \rangle$$

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_D \left(-P \underline{\frac{\partial g}{\partial x}} - Q \underline{\frac{\partial g}{\partial y}} + R \right) dA$$

Ex. Compute the flux of the vector field $\vec{F}(x, y, z) = y\vec{i} - x\vec{j} - z\vec{k}$ across the paraboloid $z = 1 - x^2 - y^2$, $z \geq 0$ oriented upward.

Solution

$$\begin{aligned}\vec{F}(x, y, z) &= \langle y, -x, -z \rangle \\ &= \langle y, -x, -1 + x^2 + y^2 \rangle.\end{aligned}$$



$$\iint_S \vec{F} \cdot d\vec{S} = \iint_D \left(-P \frac{\partial g}{\partial x} - Q \frac{\partial g}{\partial y} + R \right) dA$$

$$= \iint_D \left(-y \cdot (-2x) - (-x) \cdot (-2y) - 1 + x^2 + y^2 \right) dA$$

$$= \iint_D \left(-1 + x^2 + y^2 \right) dA = \text{polar coordinates} \dots \text{easy.} \square$$

Remark

$$\iint_{\substack{S \\ \text{oriented} \\ \text{downward}}} \vec{F} \cdot d\vec{S} = - \iint_{\substack{S \\ \text{oriented} \\ \text{upward}}} \vec{F} \cdot d\vec{S}$$



Remark $\iiint_S \vec{F} \cdot d\vec{S} = - \iint_S \vec{F} \cdot d\vec{S}$

$\downarrow$ oriented downward $\downarrow$ oriented upward

$$\vec{F} = \langle P, Q \rangle$$

Green's Th.: $\int_C P dx + Q dy = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$

$\downarrow$ closed curve in $\mathbb{R}^2$ $\downarrow$ region bounded by C

Green's Th.: $\int_C \vec{F} \cdot d\vec{r} = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$

$\downarrow$ closed curve in $\mathbb{R}^2$ $\downarrow$ region bounded by C

Generalizing Green's Th. to $\mathbb{R}^3$



$$\iiint_S \vec{F} \cdot d\vec{S} = \iiint_E ? dV$$

$\downarrow$ closed surface $\downarrow$ solid region

$$\int_C \vec{F} \cdot d\vec{r} = \iint_S ? dS$$

$\downarrow$ closed curve in $\mathbb{R}^3$ $\downarrow$ surface bounded by C

Generalizing Green's Th. to $\mathbb{R}^3$

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E ? dV$$

closed surface in $\mathbb{R}^3$ solid bounded by S

$$\int_C \vec{F} \cdot d\vec{r} = \iint_S ? dS$$

closed curve in $\mathbb{R}^3$ surface bounded by C

Divergence Th.
(Gauss-Ostrogradsky)

Stokes Th.

Divergence Theorem

Def. Suppose $\vec{F} = \langle P, Q, R \rangle$ is a vector field in $\mathbb{R}^3$.
The divergence of $\vec{F}$ is a f-n of 3 variables defined by

$$\text{div } \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

Ex. Compute the divergence of

$$\vec{F}(x, y, z) = \underbrace{(\cos x + e^y)}_P \vec{i} + \underbrace{e^{xz}}_Q \vec{j} - \underbrace{e^z \cos y}_R \vec{k}$$

Solution

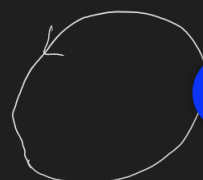
$$\text{div } \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

$$= -\sin x - e^z \cos y$$

□



Green's th.:



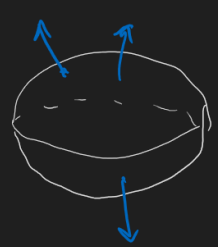
positively oriented curve.

Divergence th.:

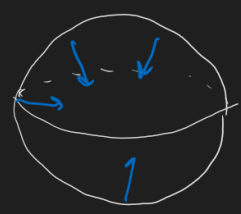
closed positively-oriented surfaces.

S is closed if it is a boundary of a solid.

S is positively oriented if at each pt of S we choose the unit normal vector pointing outside.



positive orientation



negative orientation.

Divergence Th. (Gauss-Ostrogradsky) Suppose E is a solid bounded by a surface S given with the positive orientation. Suppose $\vec{F}$ is a vector field in $\mathbb{R}^3$. Then

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E \underline{\text{div } \vec{F}} \, dV.$$



Ex. Find the flux of the vector field $\vec{F}(x, y, z) = z\vec{i} + y\vec{j} + x\vec{k}$ across the unit sphere.

Solution. Usual way: $\iint_S \vec{F} \cdot d\vec{S} = \iint_D \vec{F} \cdot (\vec{r}_\varphi \times \vec{r}_\theta) dA$.
— long way.

Instead use Divergence Th.

$$\operatorname{div} \vec{F} = 0 + 1 + 0 = 1$$

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_{\text{unit ball}} 1 \, dV = \text{volume of unit ball} = \frac{4\pi}{3} \quad \square$$



Remark. Unless stated otherwise, a closed surface is assumed to have positive orientation.

Ex. Compute $\iint_S \vec{F} \cdot d\vec{S}$, where

$$\vec{F}(x, y, z) = yz^3\vec{i} - e^{xz}\cos z\vec{j} + e^{xy}\sin x\vec{k}$$

← a closed surface is assumed to have positive orientation

Ex. Compute $\iint_S \vec{F} \cdot d\vec{S}$, where

$$\vec{F}(x, y, z) = \underbrace{yz^3}_{P} \vec{i} - \underbrace{e^{xz} \cos z}_{Q} \vec{j} + \underbrace{e^{xy} \sin x}_{R} \vec{k}$$

and S is the surface of the region bounded by the cylinder $x^2 + y^2 = 1$ and the planes $z = 0$ and $z = 1$.

Solution

$$\operatorname{div} \vec{F} = 0 + 0 + 0 = 0.$$

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E \operatorname{div} \vec{F} \, dV = 0. \quad \square$$

