



Previous lecture:



TS



$$\iint_S \vec{F} \cdot d\vec{S} \stackrel{\text{def}}{=} \iint_S \vec{F} \cdot \vec{n} \, dS =$$

flux of $\vec{F}$
across S

formula for
computation

$$= \iint_D \vec{F}(\vec{r}(u,v)) \cdot (\vec{r}_u \times \vec{r}_v) \, dA$$

Phys. sense: rate of flow of
some fluid (or heat...)
across the surface.

Divergence Th.

$$\iint_S \vec{F} \cdot d\vec{S} = \iiint_E \text{div } \vec{F} \, dV$$

closed
positively oriented
surface

solid
bounded by S

$$\vec{F} = \langle P, Q, R \rangle$$

$$\text{div } \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

$$\text{div } \vec{F} = \frac{\partial}{\partial x} + \frac{\partial}{\partial y} + \frac{\partial}{\partial z}$$

Green's Th. : $\int_C \vec{F} \cdot d\vec{r} = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$

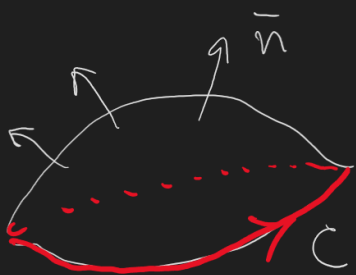
$\int_C$: closed positively oriented
 $\iint_D$: region bounded by C

Stokes' Theorem.

Def. If $\vec{F} = P\vec{i} + Q\vec{j} + R\vec{k}$ is a vector field, then the curl of $\vec{F}$ is the vector field defined by

$$\text{curl } \vec{F} = \left(\frac{\partial R}{\partial y} - \frac{\partial Q}{\partial z} \right) \vec{i} + \left(\frac{\partial P}{\partial z} - \frac{\partial R}{\partial x} \right) \vec{j} + \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) \vec{k}$$

Why called the curl : if $\vec{F}$ is a velocity field of some fluid, then curl $\vec{F}$ contains info about rotations (whirlpools). Namely, the axis about which whirlpool rotates



Suppose C is the boundary curve of S . We choose

orientation of C such that it agrees with orientation of S in the following sense: when we walk along C in the positive direction with head pointing in the direction of $\bar{n}$, S should be on our 'left'.

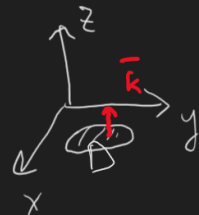
Stokes' Theorem

Suppose C is the boundary curve of S and orientations of C and S agree. Then

$$\int_C \bar{F} \cdot d\bar{r} = \iint_S \text{curl } \bar{F} \cdot d\bar{S}$$

Suppose C is a plane curve and S is a flat region.

$\bar{F}$ is a v-z field in $\mathbb{R}^3$.

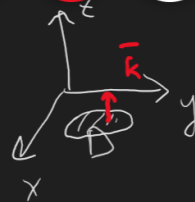


$$\bar{F}(x, y, z) = \langle P(x, y), Q(x, y), 0 \rangle$$

Left-hand side of Stokes: $\int P dx + Q dy$

Suppose C is a plane curve
is a flat region.

$\vec{F}$ is a v-z field in $\mathbb{R}^2$.



$$\vec{F}(x, y, z) = \langle P(x, y), Q(x, y), 0 \rangle$$

Left-hand side of Stokes: $\int_C P dx + Q dy$

Right-hand side of Stokes: $\iint_D \langle 0, 0, \underbrace{\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}} \rangle \cdot \langle 0, 0, 1 \rangle dA$

$$= \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA.$$

Therefore Green's Th. is a particular case of Stokes' Theorem.

Review of the course.

- Limits and continuity - definitions are the same as for f-s of 1 var., but more methods for showing $\lim_{(x,y) \rightarrow (a,b)} f$:



Review of the course.



TS



- Limits and continuity - definitions are the same as for f-s of 1 var., but more methods for showing $\lim_{(x,y) \rightarrow (a,b)} \nexists$:

approaching (x,y) along different curves should give the same limit, otherwise $\lim_{(x,y) \rightarrow (a,b)} \nexists$.

- Differentiation.

- Partial derivatives. Higher partial derivatives. $f_{xy} = f_{yx}$

- Differentiability (geometrically: tangent plane $\exists$ at each pt).

- Chain Rule. $f(x,y)$,
 $x = x(u,v)$, $y = y(u,v)$.

$$\frac{\partial f}{\partial u} = \dots, \quad \frac{\partial f}{\partial v} = \dots$$

- Gradient $\nabla f = \langle f_x, f_y \rangle$



• Differentiation.

• Partial derivatives. Higher partial derivatives. $f_{xy} = f_{yx}$

• Differentiability (geometrically: tangent plane $\exists$ at each pt).

• Chain Rule. $f(x, y)$,
 $x = x(u, v)$, $y = y(u, v)$.

$$\frac{\partial f}{\partial u} = \dots, \quad \frac{\partial f}{\partial v} = \dots$$

• Gradient $\nabla f = \langle f_x, f_y \rangle$

• Directional derivatives

$$D_{\vec{u}} f = \nabla f \cdot \vec{u}$$

unit vector

• Max/min

• local max/min occur in critical pts (that is pts at which $\boxed{\nabla f = 0}$ or $\nabla f \nexists$.)

• Max/min

- local max/min occur in critical pts (that is pts at which $\nabla f = 0$ or $\nabla f = 0$.)

2nd Derivative Test.

- absolute (global) max/min.

Extreme Value Th.: they $\exists$ on a closed bounded set.

How to find?

They can be either at critical pts or on the boundary.

How to find abs. max/min on the boundary? Either it is easy or

we use

- Lagrange Multiplier Method.

• Integration.

Integration.

- Double integrals of f-s of 2 var. over regions in $\mathbb{R}^2$.

$$\iint_D f(x,y) dA = \int \int f(x,y) \begin{matrix} dx dy \\ dy dx \end{matrix}$$

order depends on D.

$$\text{area of } D = \iint_D dA.$$

- change of variables in double int-s (Jacobian).

- polar coordinates

$$\iint_D f(x,y) dA = \iint_D \dots r \begin{matrix} dr d\theta \\ d\theta dr \end{matrix}$$

- Triple integrals of f-s of 3 var. over solids in $\mathbb{R}^3$.

$$\iiint_E f(x,y,z) dV = \int \int \int f(x,y,z) \begin{matrix} dx dy dz \\ dz dx dy \end{matrix}$$

$$\text{volume of } E = \iiint_E dV.$$



$$\text{volume of } E = \iiint_E dV$$

$$\text{mass of } E = \iiint_E \rho(x, y, z) dV$$

density f-n.

(x_0, y_0, z_0) - center of mass of E .

$$x_0 = \frac{\iiint_E x \rho(x, y, z) dV}{\text{mass}}, \quad y_0 = \dots, \quad z_0 = \dots$$

In particular case when E lies under the graph of f above region D in (x, y) -plane,

$$\text{volume of } E = \iint_D f(x, y) dA$$

• Change of variables (Jacobian).

• Spherical coordinates

$$\iiint_E f(x, y, z) dV = \iiint_E \dots \boxed{\rho^2 \sin \varphi} d\rho d\varphi d\theta$$

order depends on E .



TS



- Line integrals (integrals over curves).
Can integrate a f-n of 2 var. over a plane curve
and a f-n of 3 var. over a space curve.

Suppose C is given by parametrization
 $\vec{r}(t) = \langle x(t), y(t), z(t) \rangle, \quad a \leq t \leq b.$

$\int_C f \, ds$
 $\xleftarrow{\text{f-n for computing}}$
 $\int_a^b f(\vec{r}(t)) |\vec{r}'(t)| \, dt$

mass of C where C is made of material of density f .

length of $C = \int_C ds = \int_a^b |\vec{r}'(t)| \, dt.$

$\int_C f \, dx$
 $\xleftarrow{\text{f-n for computing}}$
 $\int_a^b f(\vec{r}(t)) x'(t) \, dt$

$\int_C f \, dy = \int_a^b f(\vec{r}(t)) y'(t) \, dt$

Therefore computing line integrals
 reduces to computing usual integrals
 of f-n of 1 var.

- Integrals of vector fields over curves

• Integrals of vector fields over curves
 $\vec{F} = \langle P, Q \rangle$ or $\langle P, Q, R \rangle$, then

work done by force fields $= \int_C \vec{F} \cdot d\vec{r} = \int_C P dx + Q dy (+ R dz).$

Conservative v-z fields, Fund. Th. for line int-s:
 $\int_C \nabla f \cdot d\vec{r} = f(z(b)) - f(z(a)).$
 Independence on path.

Green's Th.: $\int_{\text{closed } C} \vec{F} \cdot d\vec{r} \equiv \int_C P dx + Q dy$
 $= \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$

area of $D = \int_C x dy = - \int_C y dx = \frac{1}{2} \int_C x dy - y dx.$
 boundary curve of D

• Integrals over surfaces.

• Integrals of f -s of 3 var. over surfaces.

• Integrals over surfaces

• Integrals of f-s of 3 var. over surfaces.

$\vec{r}(u,v)$ - param - n of S .

$$\oint_S f(x,y,z) dS \stackrel{\text{f-la}}{=} \iint_D f(\vec{r}(u,v)) |\vec{r}_u \times \vec{r}_v| dA$$

area of $S = \iint_S dS$

If S is a graph, we get simpler f-la:

$$\oint_S f(x,y,z) dS = \iint_D f(x,y,z(x,y)) \sqrt{1+z_x^2+z_y^2} dA.$$

• Surface int-s of vector fields.

• Divergence Theorem.